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engineering

Welcome

Engineering Insights 2008

Reduced Order Models for Airflows in Buildings

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Outline

- **Design of Naturally Cool Buildings: A Lost Art?**
- **Proper Orthogonal Decomposition and Galerkin Projection**
- **Academic Example: Plane Couette Flow**
- **Industrial Example: High Performance Buildings**
- **Looking Forward**

Design of Naturally Cool Buildings: A Lost Art?

Historically, design techniques were used so that a building was naturally cool:

- **Barriers against entry of heat**
- **Massive masonry shells that absorb heat (thermal capacitors), perhaps “drain” heat to open body of water**
- **Use of “cool material”, such as marble**



Cool Buildings: Some New Ideas

Chicago City Hall roof garden: 20,000 square feet



Can keep roof as much as 70 degrees cooler,
so less energy needed to keep building cool

Cool Buildings: Some New Ideas

Zuidas section of Amsterdam



Deep water from local man-made lake used to cool another supply of water for “cold-radiators” in buildings

Provides air-conditioning for 700,000 people

Some New Ideas: Control of Airflows

- **Goal:**
the design and active control of indoor airflows to improve ventilation and efficiency of heating and cooling in buildings
- **Approach:**
develop low-dimensional models which capture enough physics to be meaningful, but which are computationally inexpensive and allow the development of control strategies

Proper Orthogonal Decomposition

- Basic Theory

- consider set of velocity snapshots $\{\mathbf{u}(\mathbf{x})\}$

- find basis of POD modes $\{\Phi\}$ which maximizes $\frac{\langle |(\mathbf{u}, \Phi)|^2 \rangle}{\|\Phi\|^2}$

- Properties of POD Modes

- orthogonality (normalization \rightarrow orthonormality)

- POD modes individually satisfy incompressibility, BCs

- optimality: for a given number of modes
energy captured by POD basis $>$ any other basis

Galerkin Projection

- write evolution PDE as

$$\frac{\partial \mathbf{u}}{\partial t} = \mathbf{F}(\mathbf{u})$$

- expand

$$\mathbf{u}(\mathbf{x}, t) = \sum_n a_n(t) \Phi_n(\mathbf{x}),$$

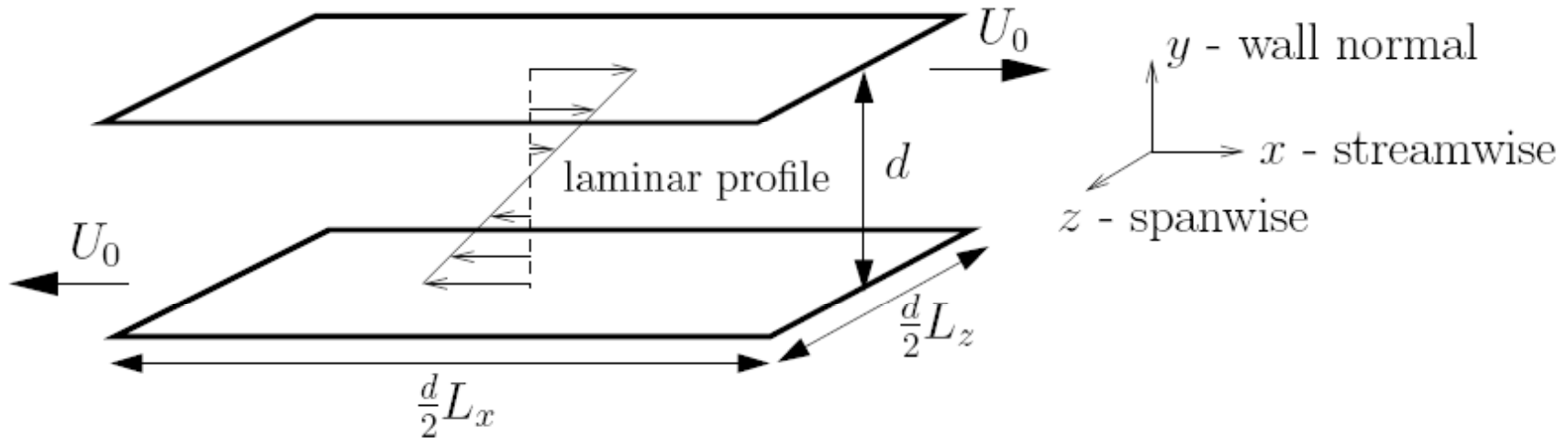
- substitute into evolution PDE

$$\sum_n \dot{a}_n(t) \Phi_n(\mathbf{x}) = \mathbf{F} \left(\sum_n a_n(t) \Phi_n(\mathbf{x}) \right)$$

- take inner product with $\Phi_m(\mathbf{x})$, use orthonormality

$$\Rightarrow \dot{a}_m(t) = \left(\mathbf{F} \left(\sum_n a_n(t) \Phi_n(\mathbf{x}) \right), \Phi_m(\mathbf{x}) \right)$$

Academic Example: Plane Couette Flow



Nondimensional equations for perturbation to laminar state:

$$\frac{\partial}{\partial t} \mathbf{u} = -(\mathbf{u} \cdot \nabla) \mathbf{u} - y \frac{\partial}{\partial x} \mathbf{u} - v \mathbf{e}_x - \nabla p + \frac{1}{Re} \nabla^2 \mathbf{u}$$

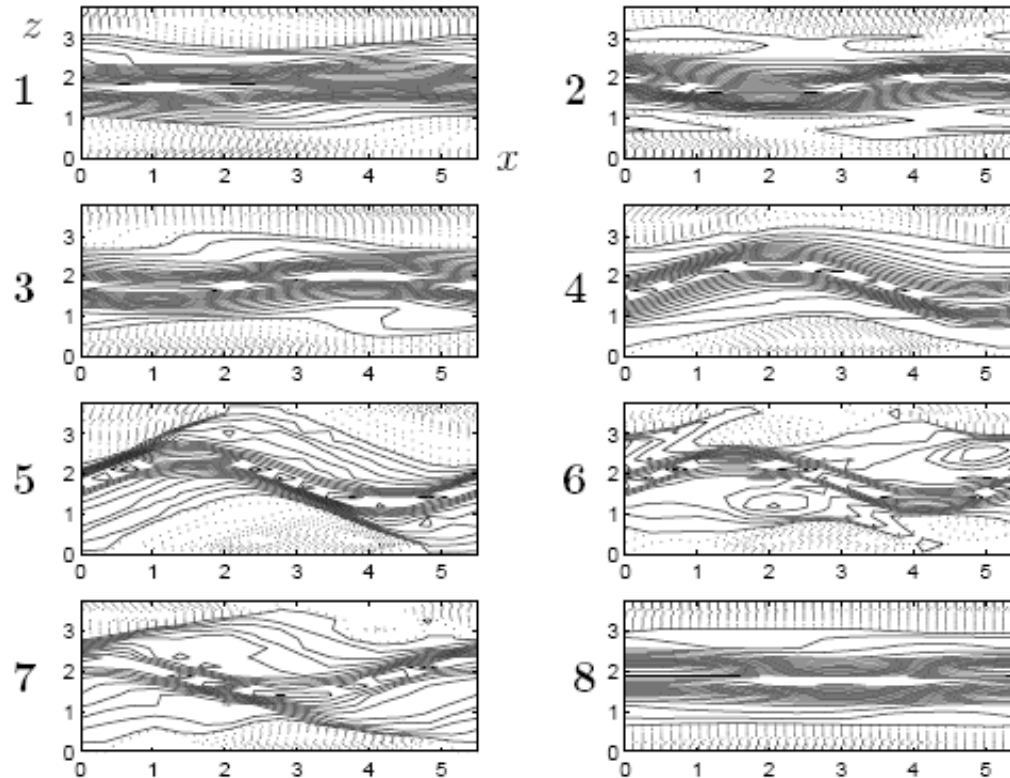
$$\nabla \cdot \mathbf{u} = 0 \quad \mathbf{u}|_{y=\pm 1} = 0 \quad Re = \frac{U_0(d/2)}{\nu}$$

Periodic Boundary Conditions in x and z

Minimal Flow Unit: $L_x = 1.75 \pi, L_z = 1.2 \pi$

- Streak Breakdown

Midplane x -velocity contours



Minimal Flow Unit: $L_x = 1.75 \pi, L_z = 1.2 \pi$

□ POD decomposition of PCF–MFU

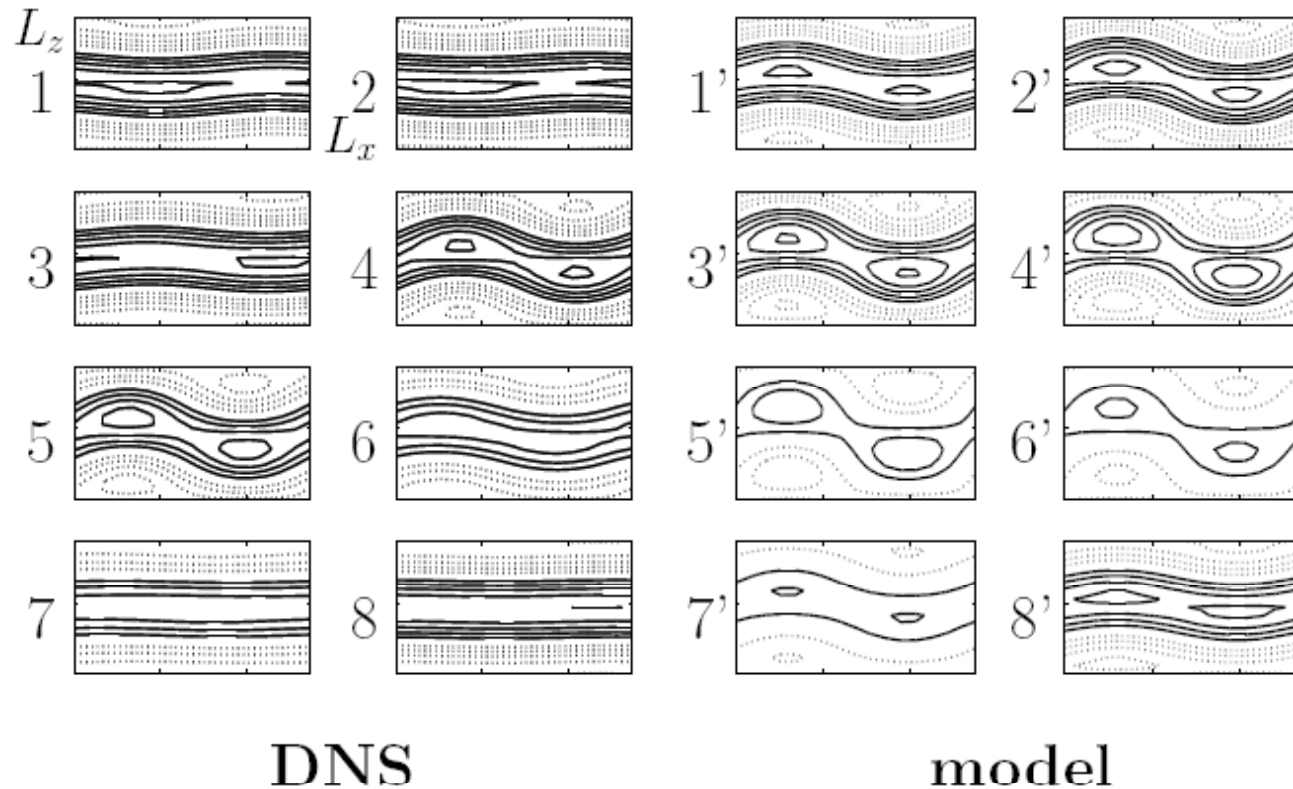
(n, n_x, n_z)	$\lambda_{n_x n_z}^{(n)}$	$\% E_{n_x n_z}^{(n)}$	Model
(1, 0, 0)	4.4550	68.02	■
(1, 0, ±1)	0.7821	23.88	■
(1, 0, ±2)	0.0543	1.66	■
(1, ±1, 0)	0.0386	1.18	■
(1, 0, ±3)	0.0195	0.59	“more of same”
(2, 0, 0)	0.0174	0.27	“exclude 2nd family”
(2, 0, ±1)	0.0123	0.38	“exclude 2nd family”
(1, ±1, ±2)	0.0109	0.33	“Fourier interactions”
(1, ±1, ±1)	0.0090	0.27	■
...			

- 11-dimensional dynamical system

Model includes terms for modes not in truncation

Minimal Flow Unit: $L_x = 1.75 \pi, L_z = 1.2 \pi$

- comparison of DNS and model
 - midplane x -velocity contours



Summary of Procedure

snapshots for PCF turbulence (DNS)



eigenvalue problem

POD modes

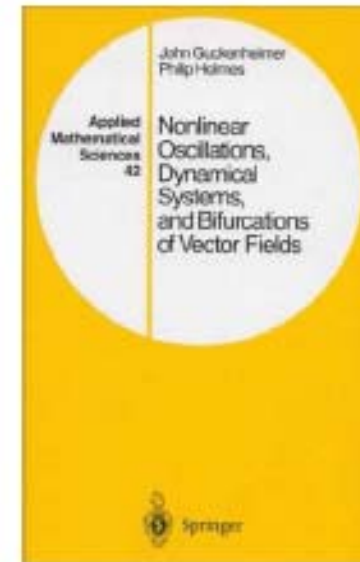


Galerkin projection, truncation

ODE models



insight into turbulence



Low-dimensional model → Control

Industrial Example: High Performance Buildings

Slides: adapted from Amit Surana (United Technologies Research Center)

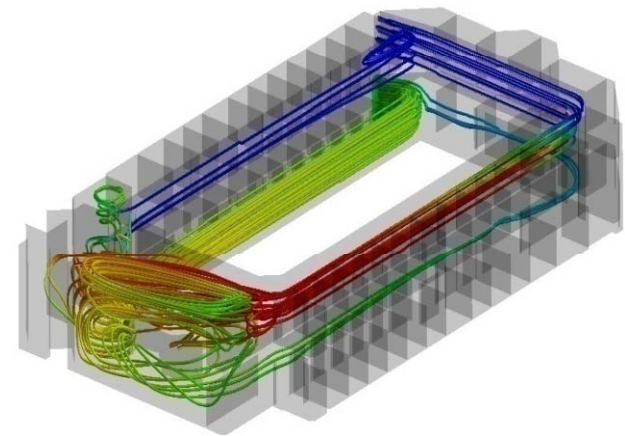
Normal Building Operations:

Optimize comfort, indoor air quality, energy efficiency

Emergency Operations:

Real-time information on contaminant/smoke propagation
Support first-responders, & evacuation management

**Flow structures in large spaces
have significant effects on
transport : thermal, smoke &
contaminants**



High Performance Buildings

Role of Coherent Structures in

- 1) Mixing dynamics**
- 2) Strategies for sensing & actuation**
- 3) Reduced order modeling**
- 4) Feedback control of mixing**

High Performance Buildings

Airflow Dynamics

Boussinesq approximation,
negligible viscous dissipation

$$\begin{aligned} \nabla \cdot \mathbf{v} &= 0, \\ \rho_0 \left(\frac{\partial v_i}{\partial t} + v_i \frac{\partial v_i}{\partial x_i} \right) &= -\frac{\partial p'}{\partial x_i} - \rho_0 \beta T_d g_i + \mu \nabla^2 \mathbf{v}, \\ \rho_0 C_p \left(\frac{\partial T_d}{\partial t} + v_i \frac{\partial T_d}{\partial x_i} \right) &= k \nabla^2 T_d, \end{aligned}$$

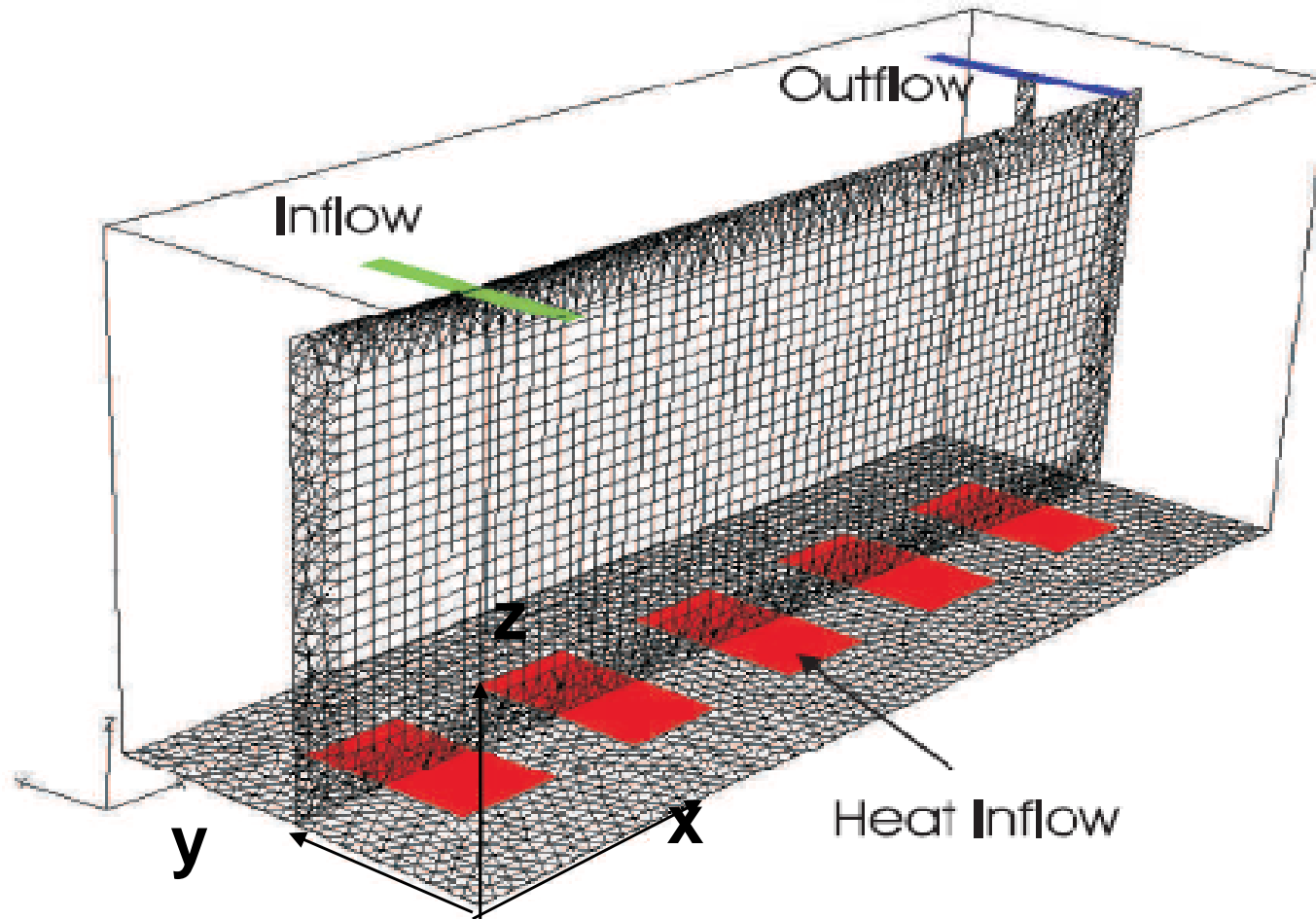
Expansion in POD Models

$$\begin{aligned} \mathbf{v}(\mathbf{x}, t) &= \mathbf{v}^0(\mathbf{x}) + \sum_{i=1}^n a_i(t) \phi_i(\mathbf{x}), \\ T(\mathbf{x}, t) &= T^0(\mathbf{x}) + \sum_{i=1}^p b_i(t) \psi_i(\mathbf{x}). \end{aligned}$$

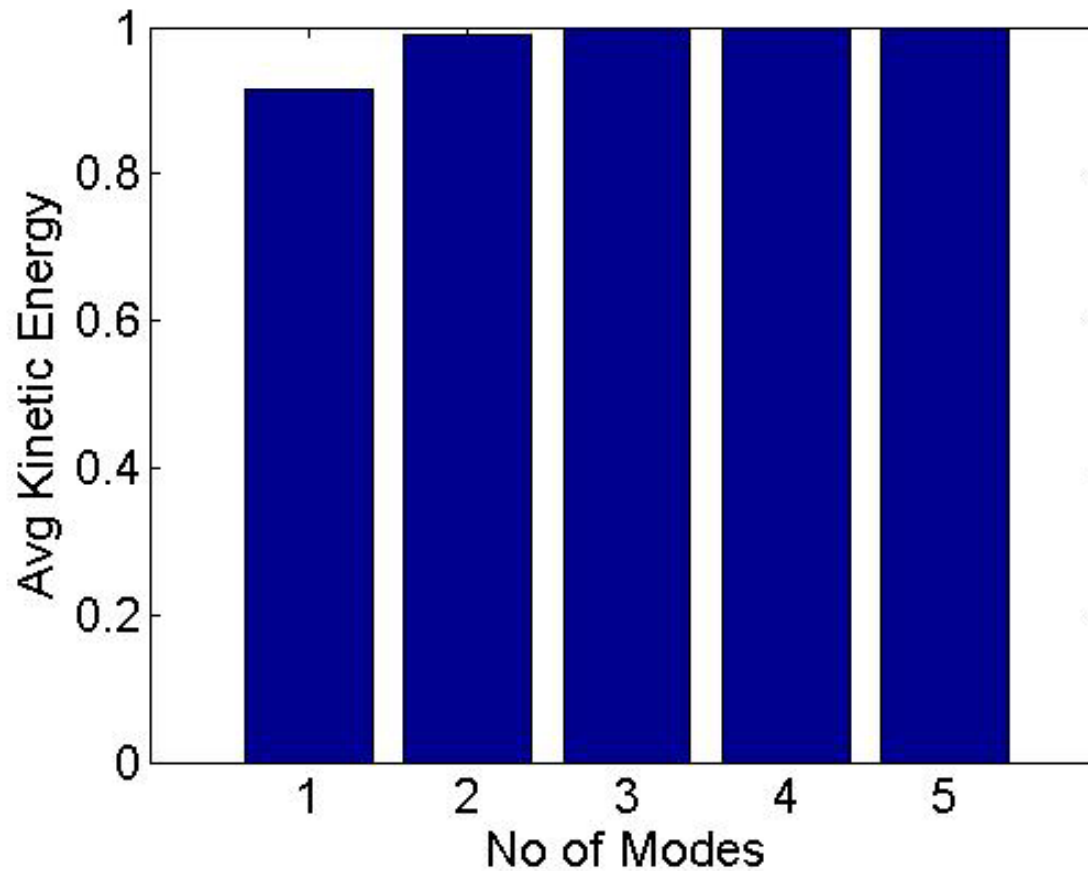
Galerkin Projection \longrightarrow Low-Dimensional Model

Initial Conditions? Sensors

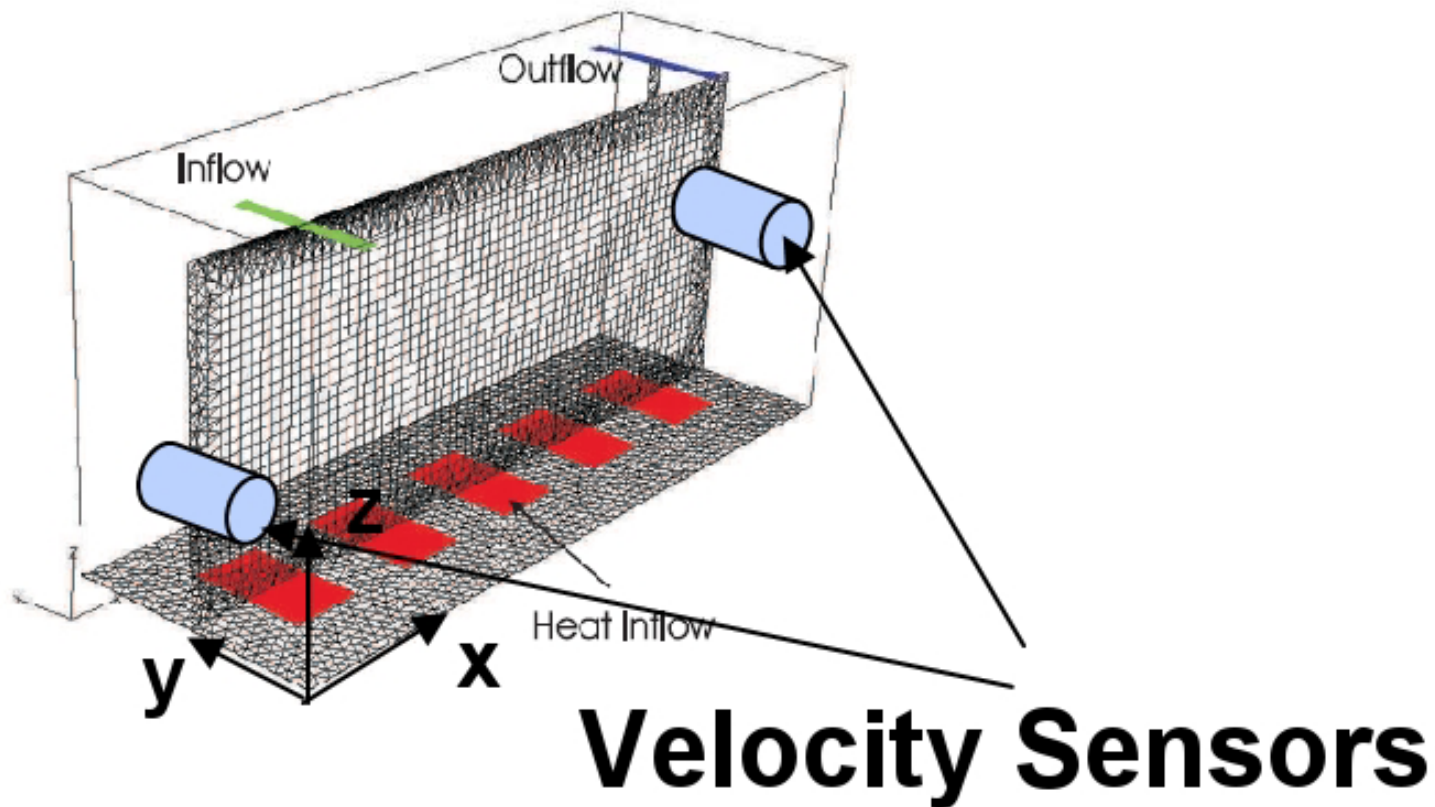
Model Reduction for 3D Room



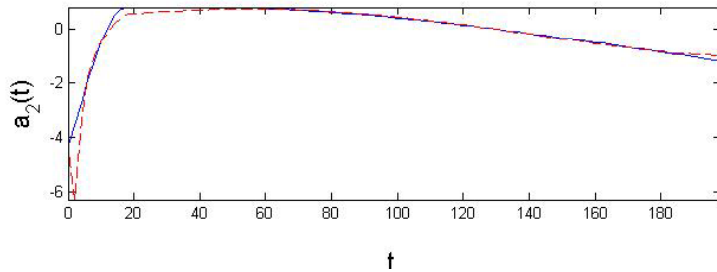
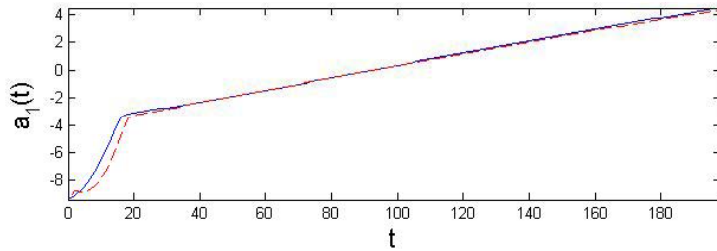
Model Reduction for 3D Room



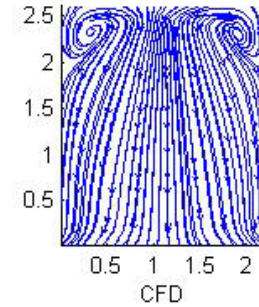
Model Reduction for 3D Room



Model Reduction for 3D Room

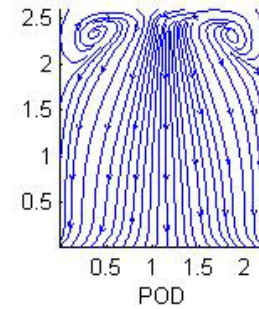


DNS

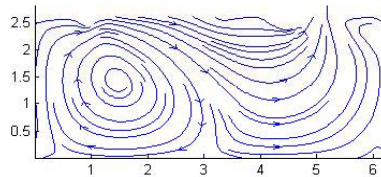


X-Slice

model

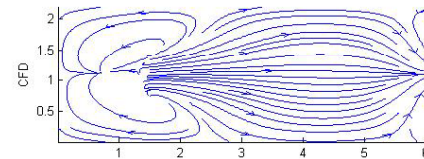


DNS



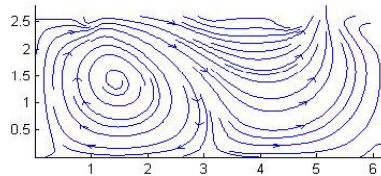
Y-Slice

DNS

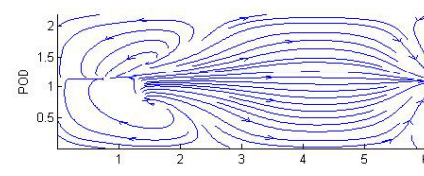


Z-Slice

model



model

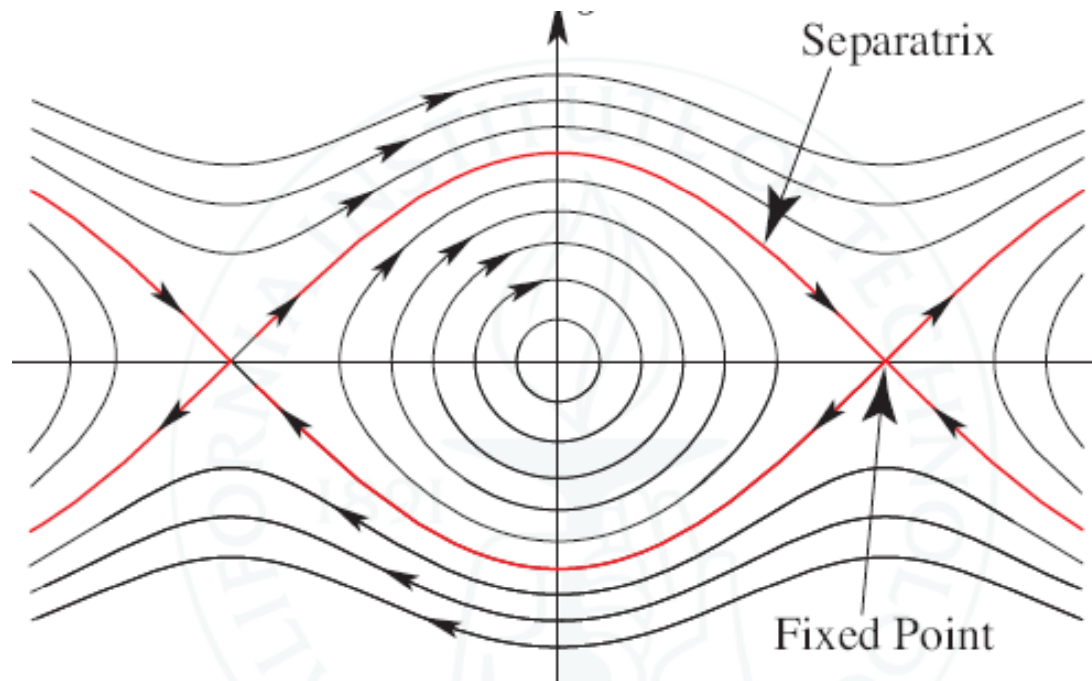


Lagrangian Coherent Structures

Underlying structures that dictate transport and mixing

Straining Regions: stretching, folding & alignment

Vortices: trap material

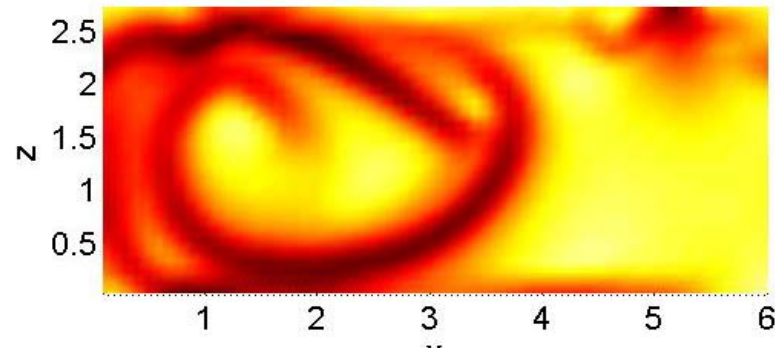


Thanks to Jerry Marsden, Caltech

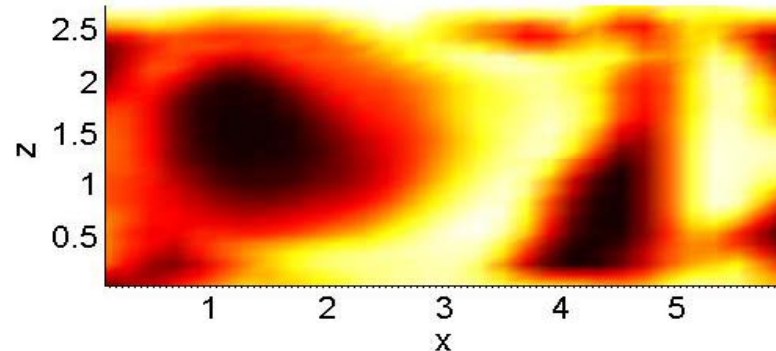
Application to Building Environment

- **Mechanical Ventilation**

DLE



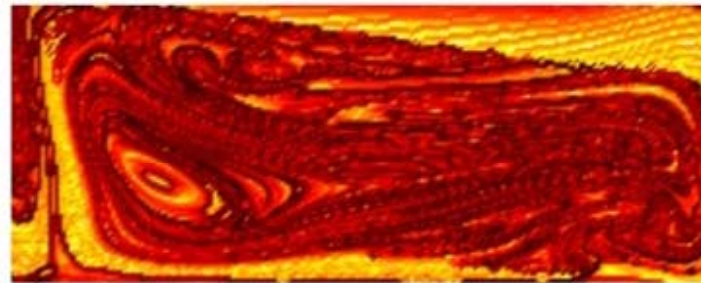
M_z



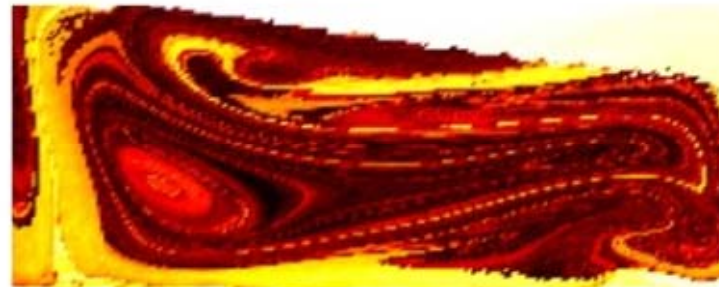
Application to Building Environment

- **Mechanical Ventilation & Moderate Heating**

DLE



M_Z



Application to Building Environment

- **Mechanical Ventilation & Continuous Heating**

DLE

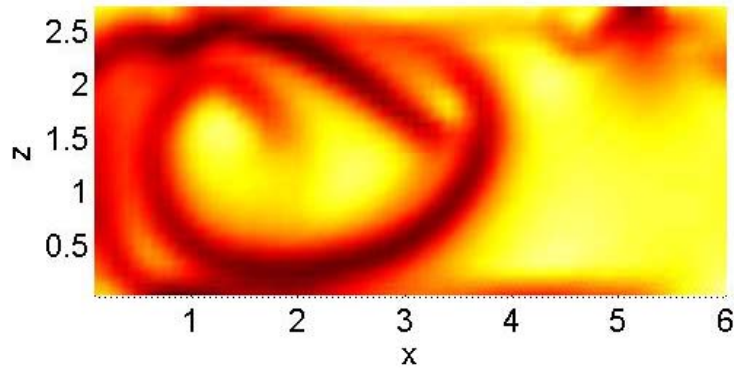


M_Z

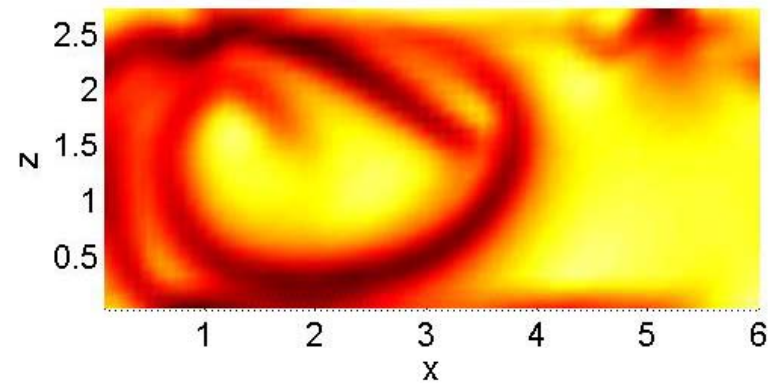


LCS Based Model Reduction

DNS



1 Mode



1 Mode is sufficient to capture transport

Looking Forward

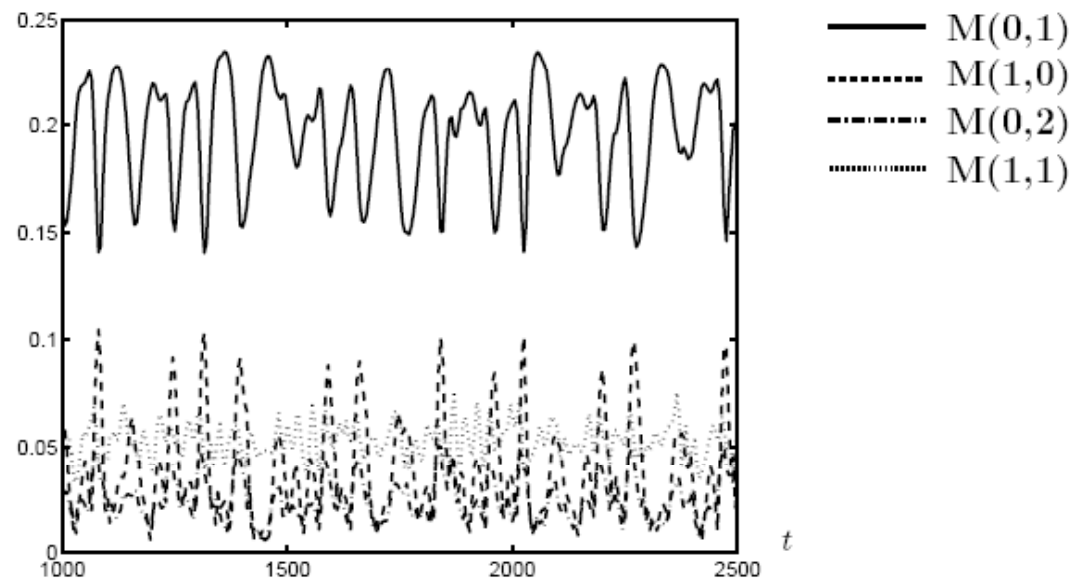
- **Better low-dimensional models:**
 - modeling loses to truncated modes
 - models which minimize error over specified time interval
 - modes based more directly on Lagrangian Coherent Structures
 - treatment of multiple rooms connected by vents/hallways

- **Optimal sensor placement and estimation**

- **Optimal control of mixing**

Minimal Flow Unit: $L_x = 1.75 \pi, L_z = 1.2 \pi$

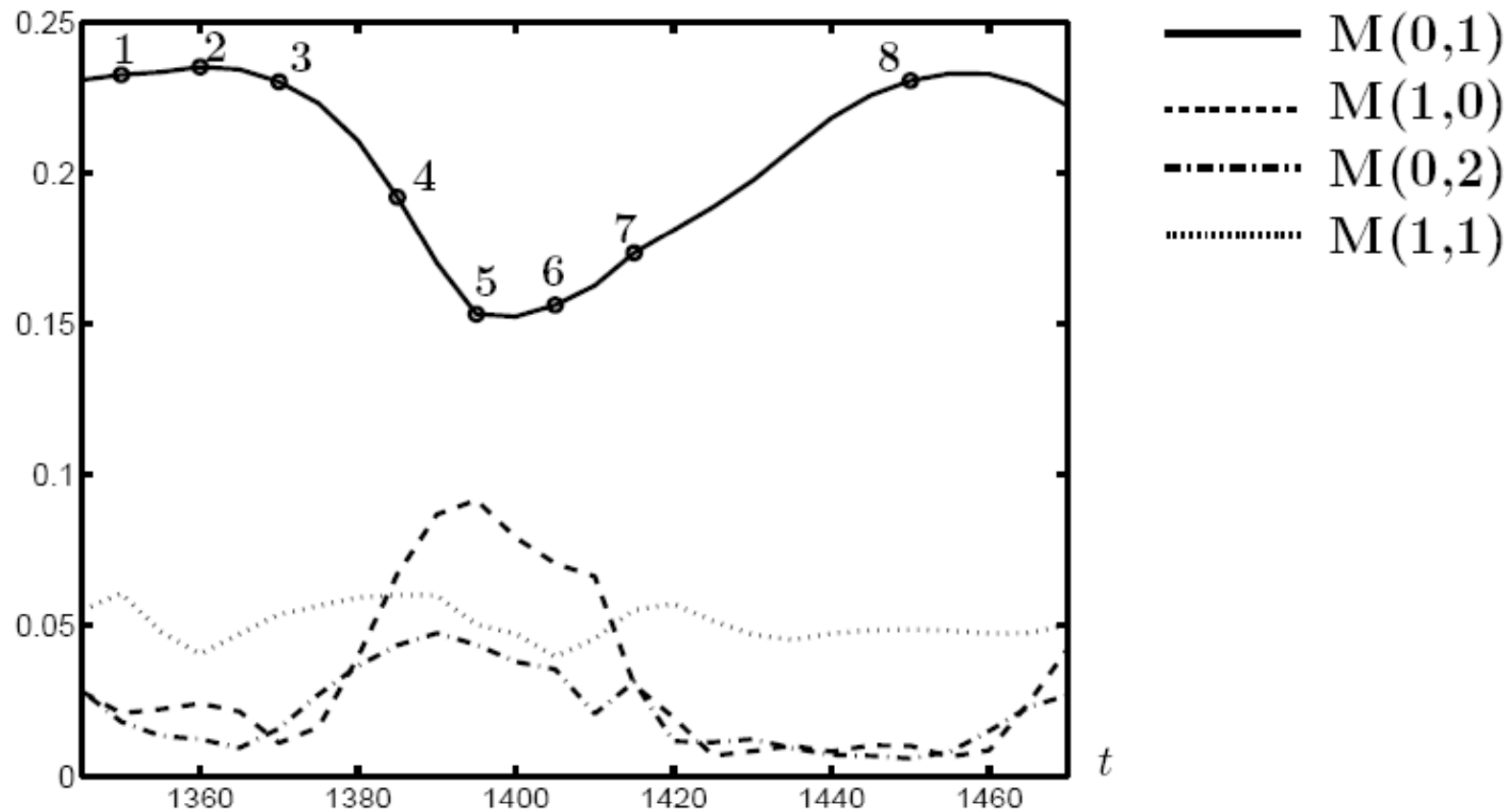
- MFU: smallest domain in which turbulence can be sustained - Hamilton, Kim, Waleffe *JFM* 1995
- define modal RMS velocity $M(n_x, n_z)$ as energy contained in wavenumbers n_x, n_z ; for $Re = 400$



- flow is roughly periodic with period 80 – 100

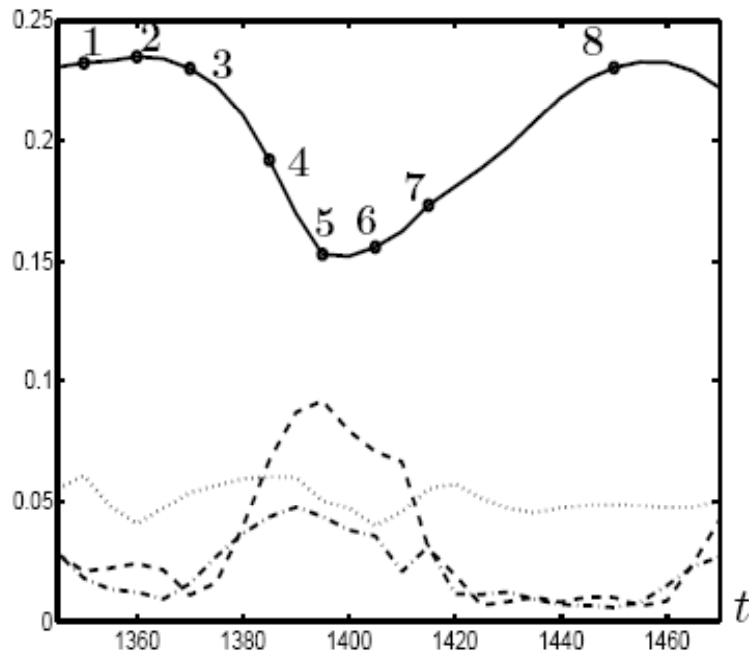
Minimal Flow Unit: $L_x = 1.75 \pi, L_z = 1.2 \pi$

- Closeup of one representative period

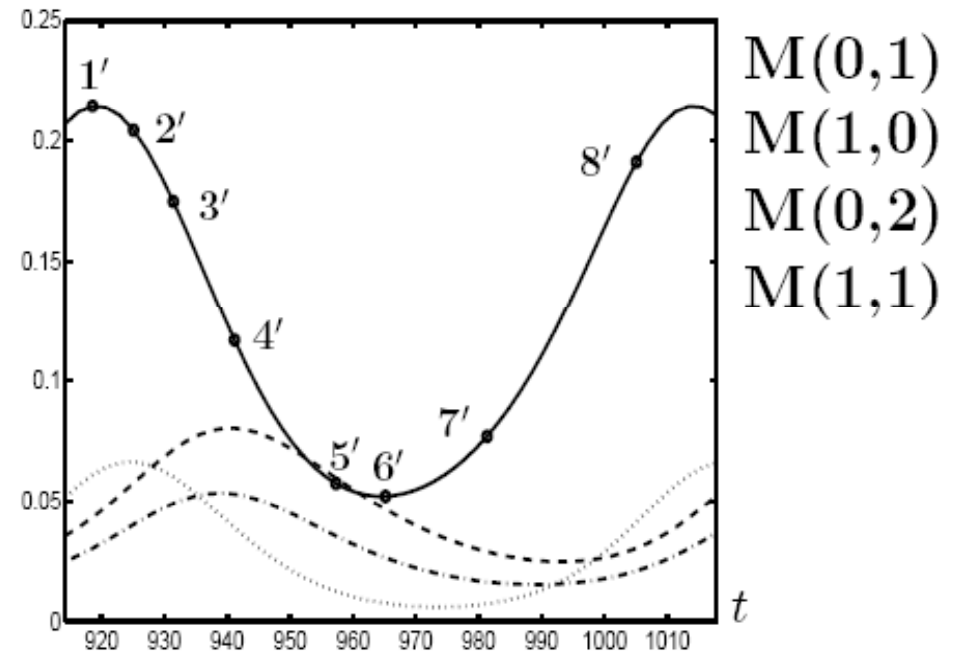


Minimal Flow Unit: $L_x = 1.75 \pi, L_z = 1.2 \pi$

- comparison of DNS and model
- RMS modal velocities



$T \approx 80 - 100$



$T = 95$