
“Valves Tapping in Rhythm”

Electro-Mechanical Valve (EMV) Actuator Control for Camless Engines

Kathy Peterson and Anna Stefanopoulou

The Mohammed Dahleh Symposium



**Powertrain
Control Lab**

Thanks to NSF (ECS-0049025), Ford Motor, and Volvo Cars

University of Michigan

Gasoline Engine Trends

“Apart from our focus on hydrogen as the fuel of the future, Valvetronic is a decisive technology in reaching our CO2 objectives in the future.”

B. Goschel, BMW



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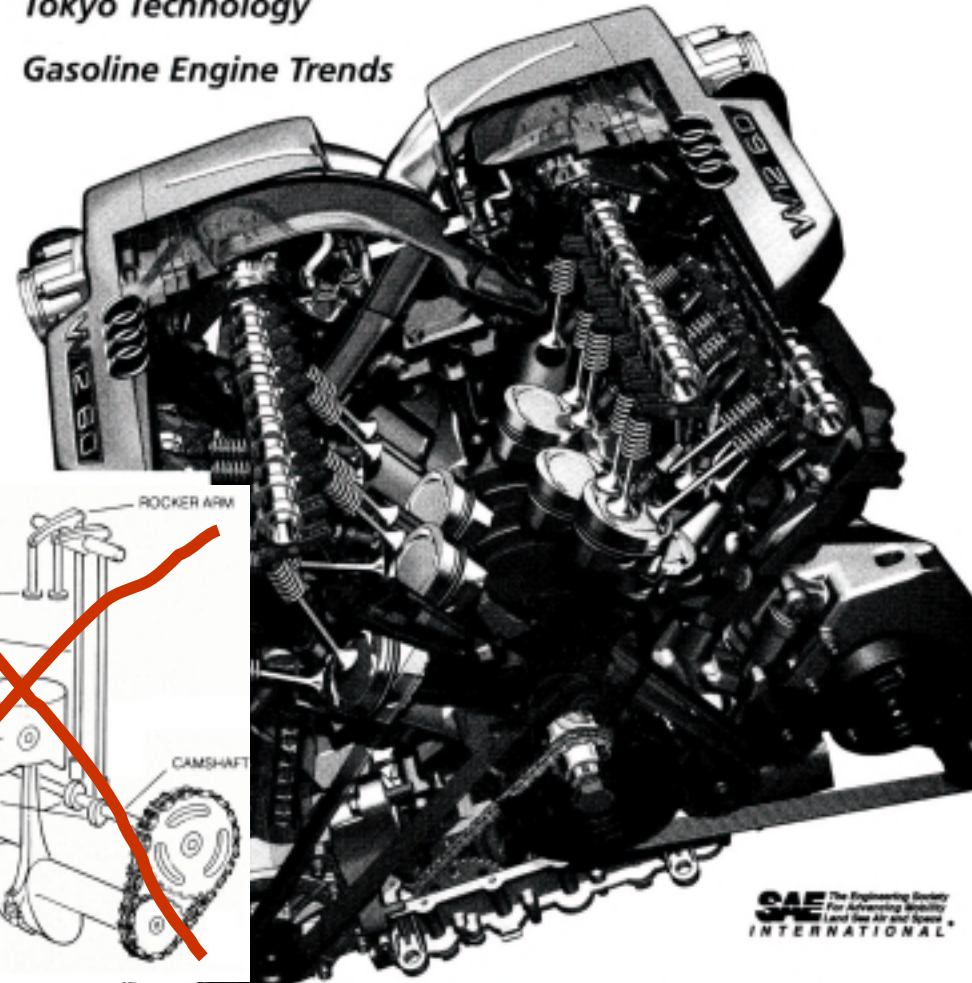
January 2002

automotive engineering

international

Tokyo Technology

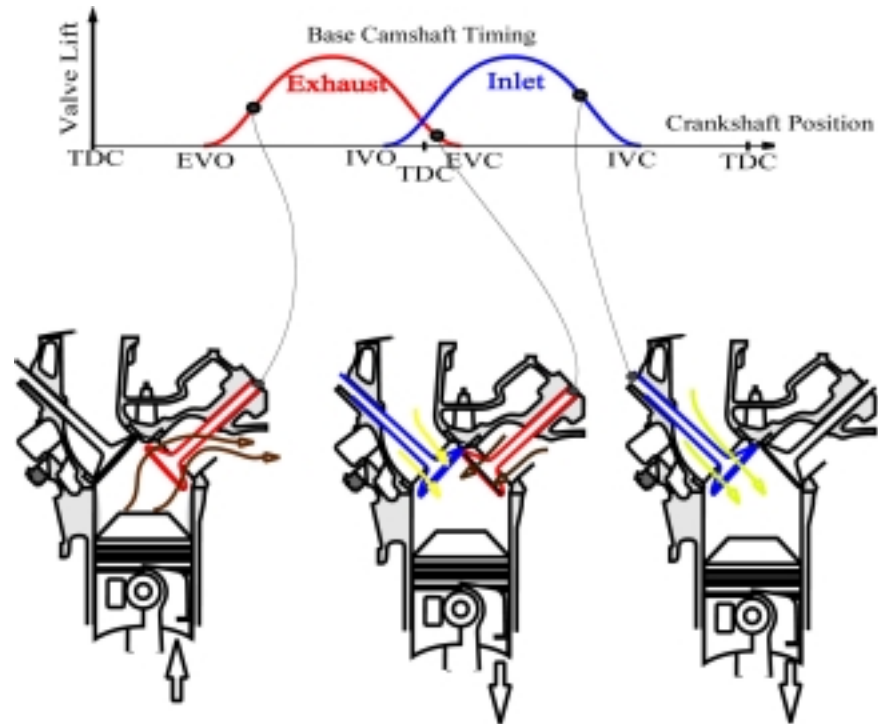
Gasoline Engine Trends



SAE The Engineering Society
For Advancing Mobility
Land Sea Air and Space
INTERNATIONAL

From Cam-Variable to Cam-Less

- **Better fuel efficiency**
 - Less pumping loss (Levin et al)
 - Cylinder deactivation (Hatano et al)
 - Improvement is up to 10-15% (Kreuter et al)
- **Increased torque output**
 - Ramming effect during high engine speed
 - Improvement is up to 20% (Hatano et al)
- **Elimination of external Exhaust Gas Recirculation (EGR)**
- **Reduced emissions**
 - Reduction of NO_x is up to 40% (Moriya et al)
 - Reduction of HC is up to 15% (Lancefield et al)
 - Reduction of CO is up to 5% (Gould et al)

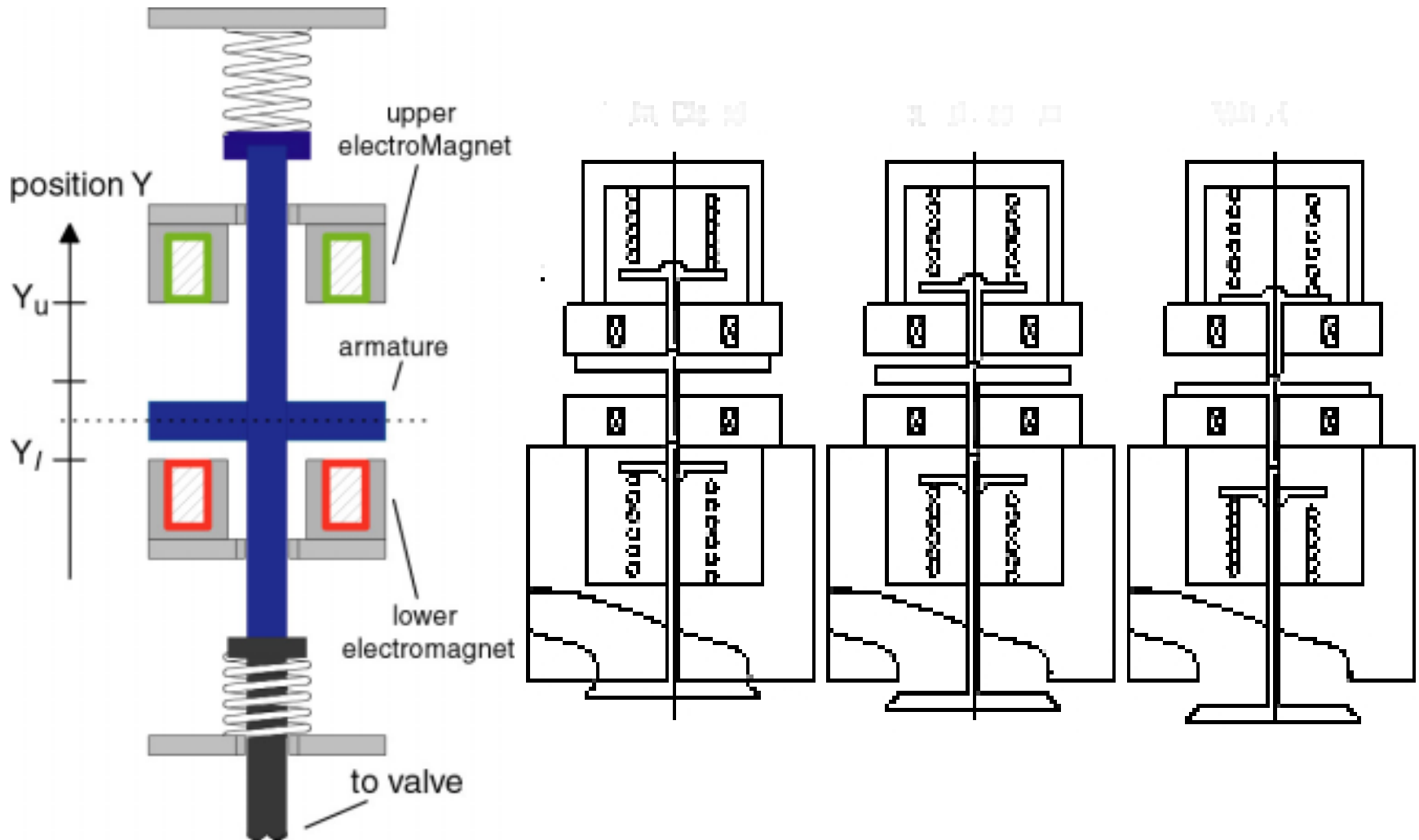


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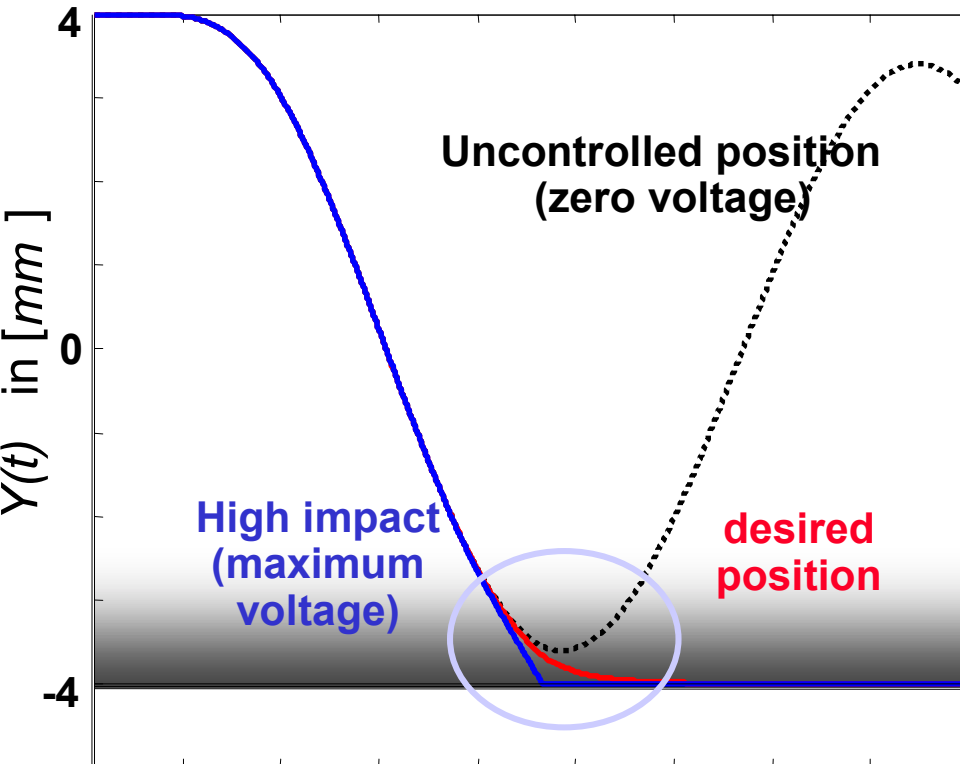
- How does the EMV actuator work
- The Control Problem
- Feedback controller
- Self-tuning



Electro-Mechanical Valvetrain (EMV)



Problem: Fast Transition and Soft Landing



PROBLEM

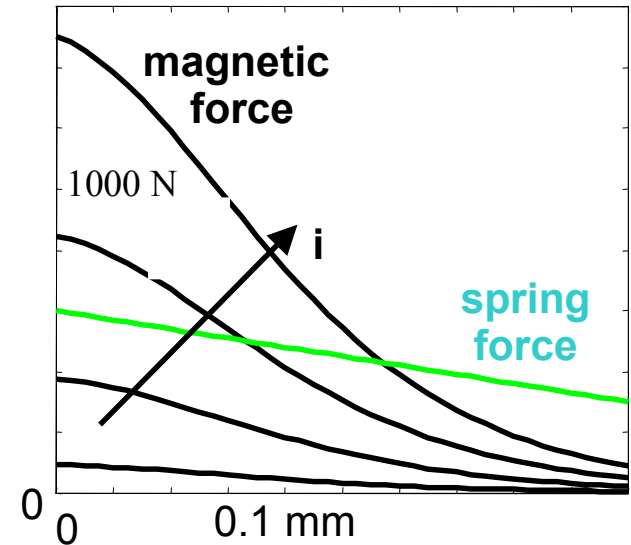
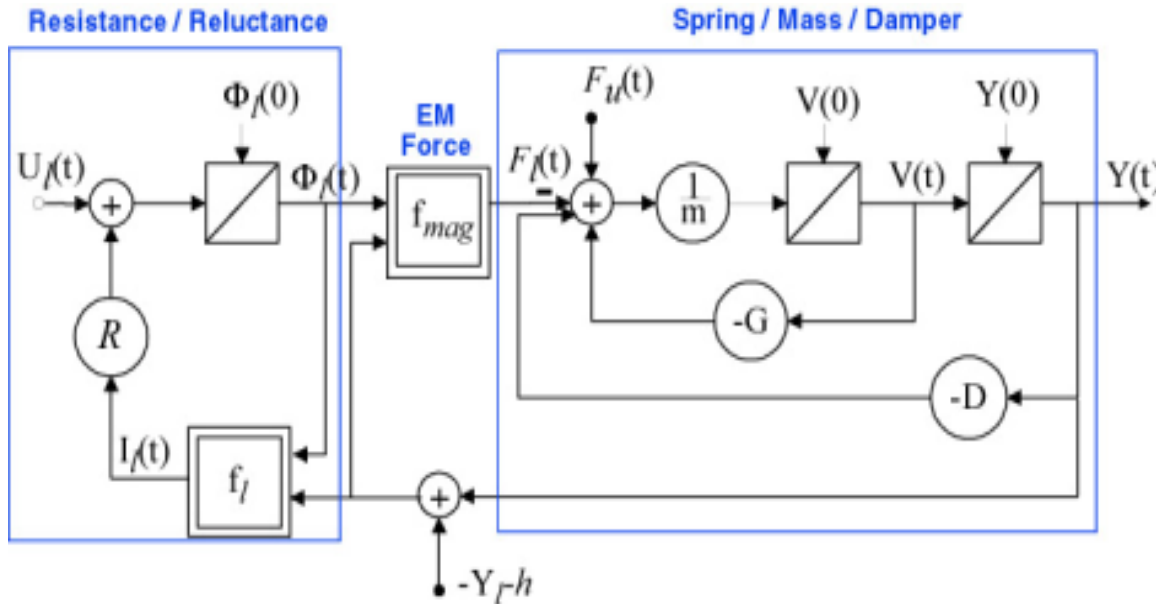
- Voltage too high: velocities $> 1\text{ m/sec}$ noise and component wear
- Voltage too low: accurate closing not ensured

GOAL

- Impact velocities of less than 0.05 m/s
- Consistent transition times of approximately 4 ms
- Rejection of disturbance due to pressure differences



Difficulties

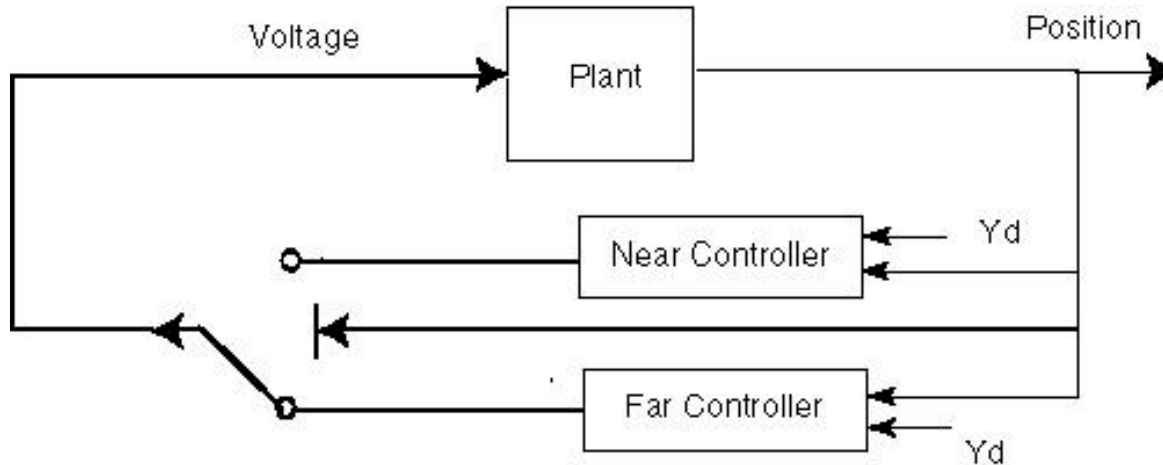


Feedback control difficulties

- Unstable system close to the contact point
- Actuator authority range and saturation
- Nonlinear magnetic force
- Uncertain system parameters close to the contact point



Linear Feedback Control design

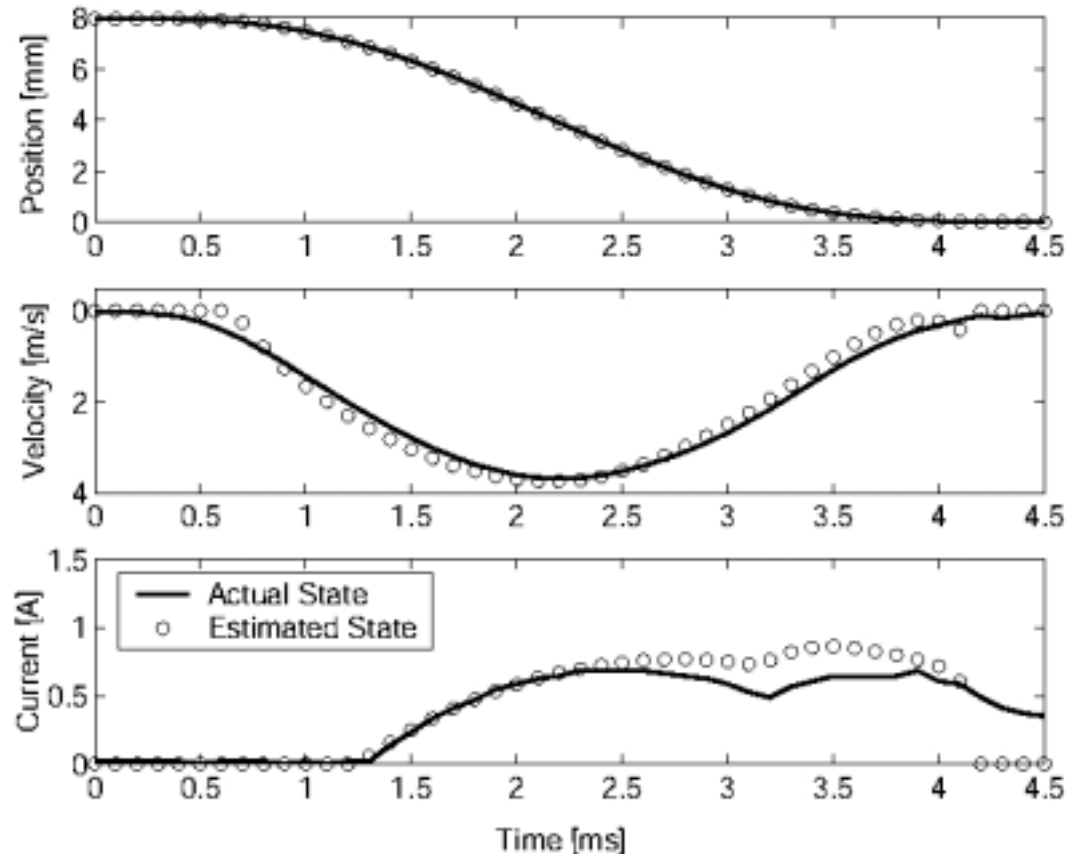


- Linearization at two equilibrium points in the transition trajectory
- Switch between two linear feedback controllers
 - Flux initialization (penalty on current)
 - Regulation (penalty on position)
- Observer for velocity and current



State Observer (+controller)

Discrete Nonlinear Reduced Order observer

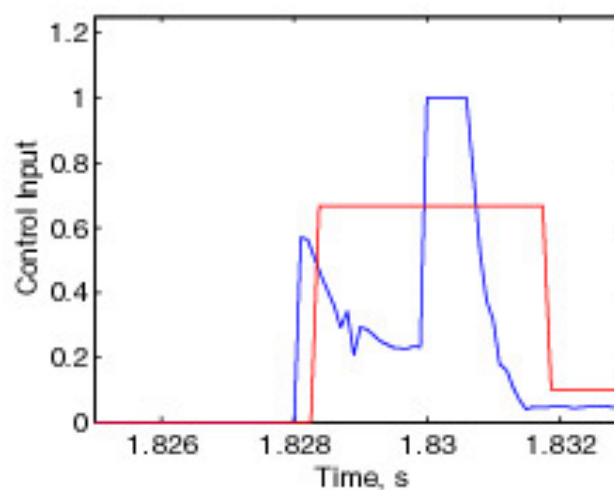
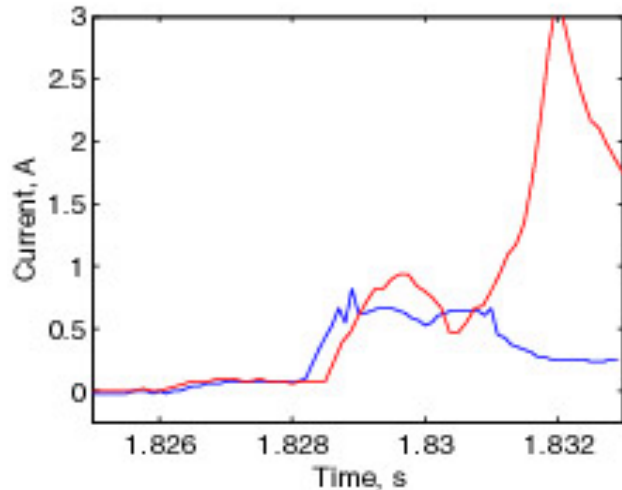
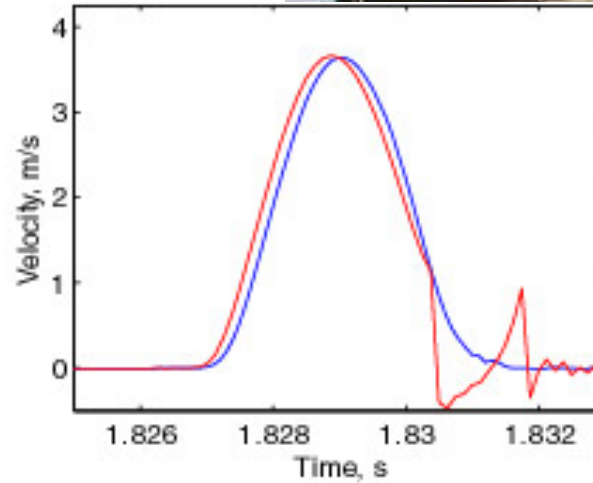
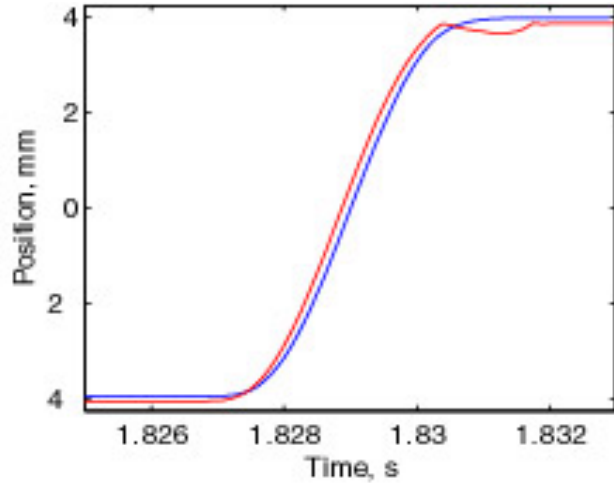
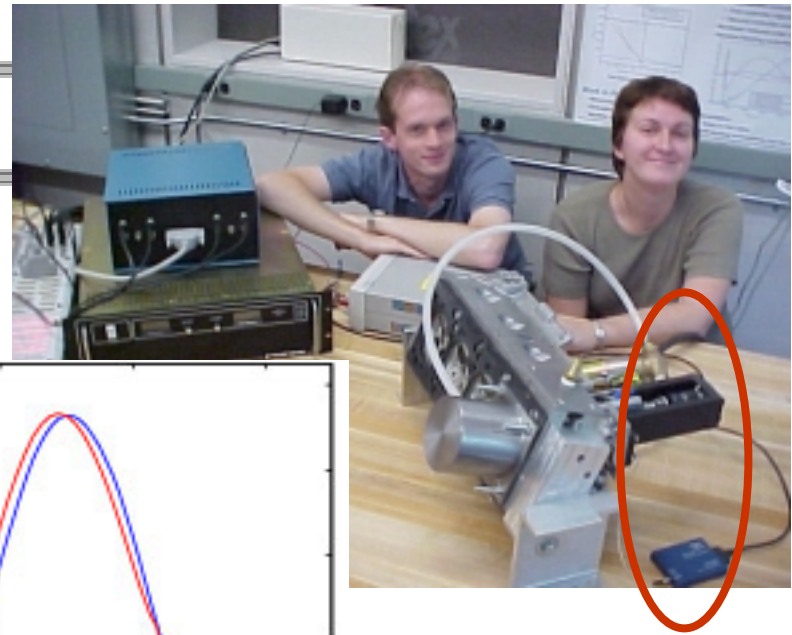


Current is nearly unobservable

- Magnetic force has weak influence on valve motion while the armature is away from the contact position
- Near the contact position, the magnetic force is more strongly influenced by changes in position than changes in current
- Sampling: 20Khz
 - **Impact Velocity**
Mean=0.15 m/s ($\sigma=0.1$ m/s)
 - **Transition Time**
Mean=3.25 ms ($\sigma=0.04$ ms)



Implementation



Thanks to:

Yan Wang (UCSB)

Garrick McNey (UCSB)

Kathy Peterson (UMICH)

Richard Kors (UMICH)

and

Brad and Lena Paden!

Looking at the Dynamics

$$\frac{di}{dt} = \frac{V_c - ri + \chi_1(z, i)v}{\chi_2(z)}$$

$$\frac{dz}{dt} = 1000v$$

$$\frac{dv}{dt} = \frac{1}{m} \left(-F_{\text{mag}}(z, i) + k_s(4 - z) - bv \right)$$

$$\chi_1 = \frac{2k_a i}{(k_b + z)^2},$$

$$\chi_2 = \frac{2k_a}{1000(k_b + z)}$$

$$F_{\text{mag}} = \frac{k_a i^2}{(k_b + z)^2}$$

$$k_b \ll 1 \quad \& \quad z \rightarrow 0$$

$$\Rightarrow \text{let } \varepsilon = k_b + z$$

$$\Rightarrow \varepsilon \frac{di}{dt} = 1000 \left(\frac{(V_c - ri)\varepsilon^2}{2k_a} + iv \right)$$

Effects:

- Loss of Control Authority
- Current becomes singularly perturbed

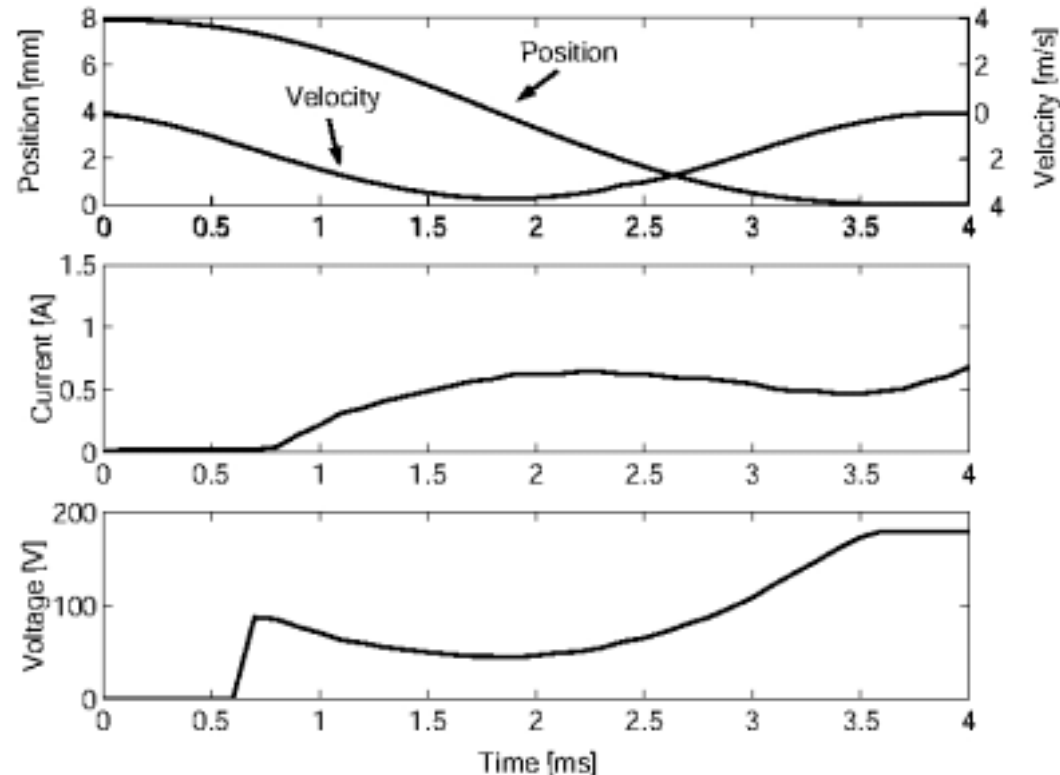


Nonlinear Controller

$$V_c = \frac{K_1}{\gamma + z} v + \frac{K_2}{\beta + \frac{z}{\kappa}}$$

Addresses:

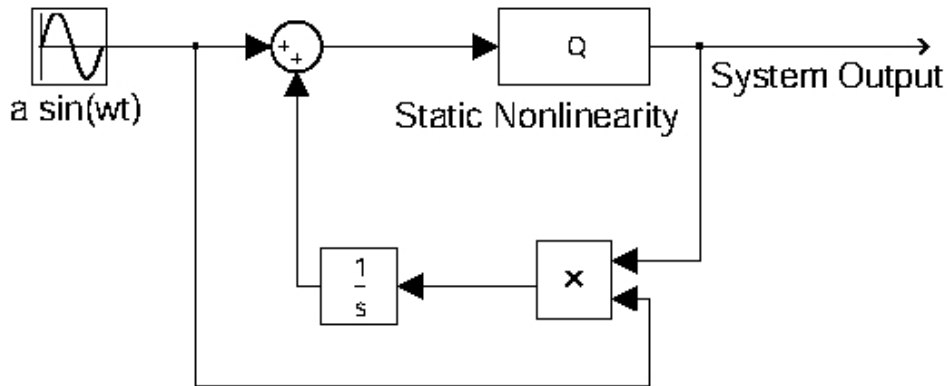
- ✓ Loss of Control Authority
The feedback is inversely proportional to the position
- ✓ Impact
The voltage is controlled to account potential bouncing



- **Impact Velocity**
Mean=0.16 m/s ($\sigma=0.08$ m/s)
- **Transition Time**
Mean=3.23 ms ($\sigma=0.04$ ms)
- **Factor of 6 reduction in impact velocity**



Extremum Seeking Controller

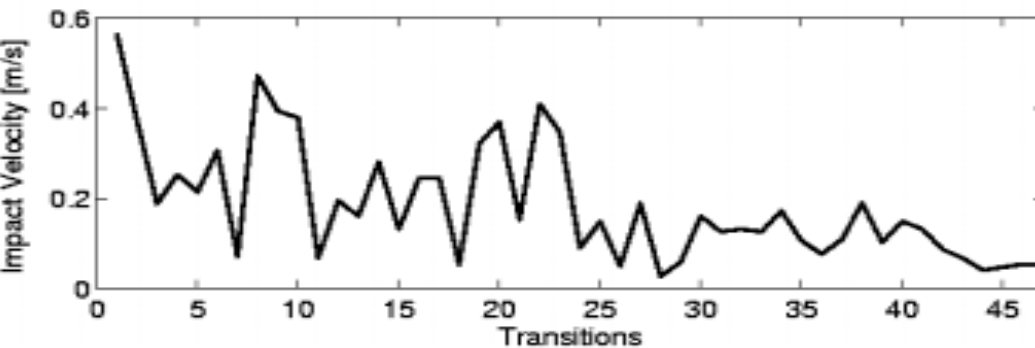
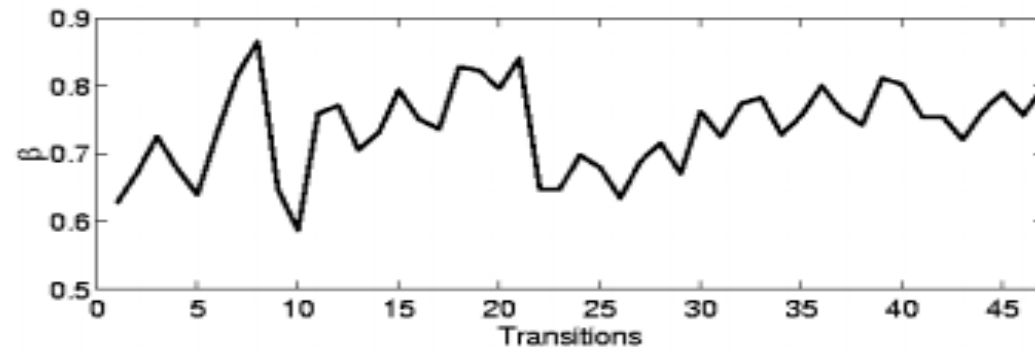
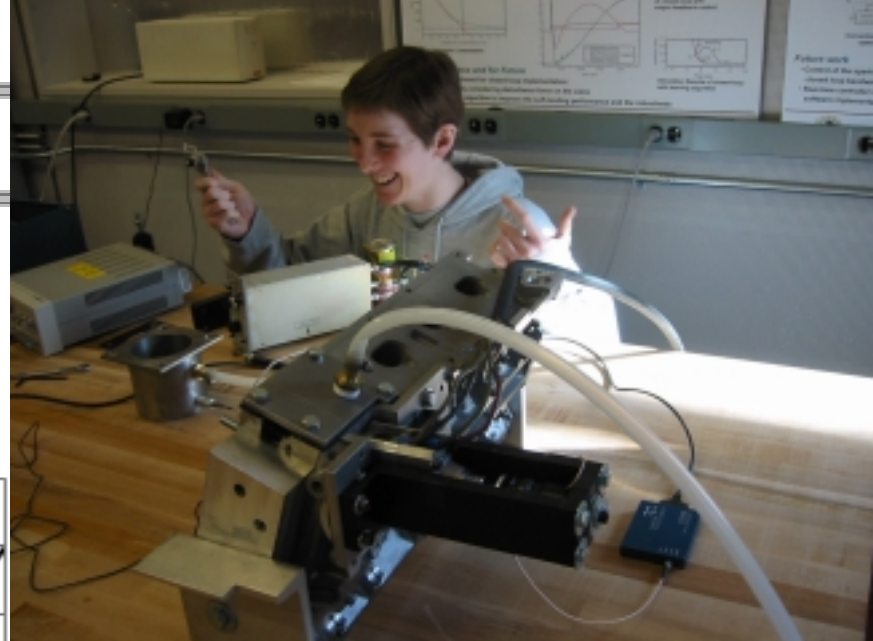


- Extremum seeking control is used to drive the output of a static nonlinearity to a local maximum or minimum
- The system can be treated as a static nonlinearity by viewing
 - The parameter β as the input
 - The function:

$(0.05 - v_I)^2$
as the output



Experimental Results



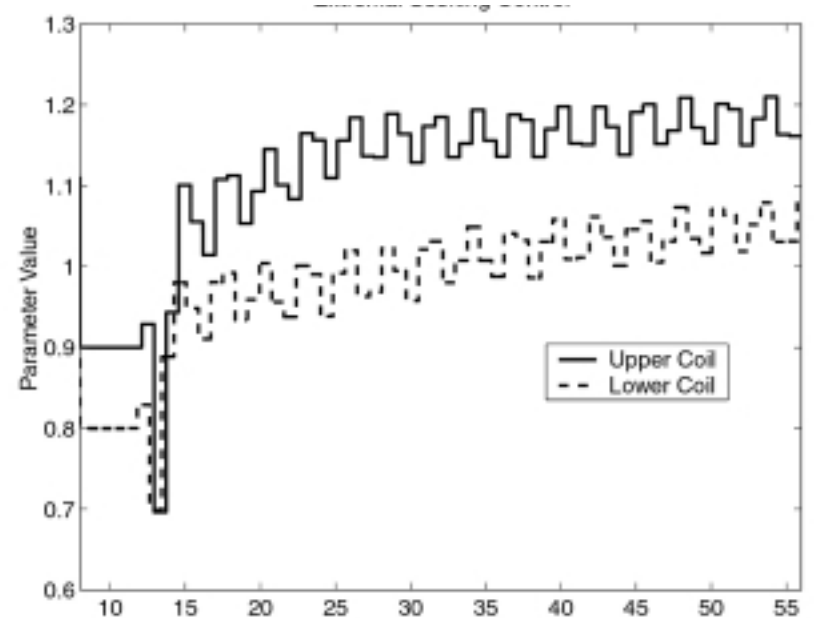
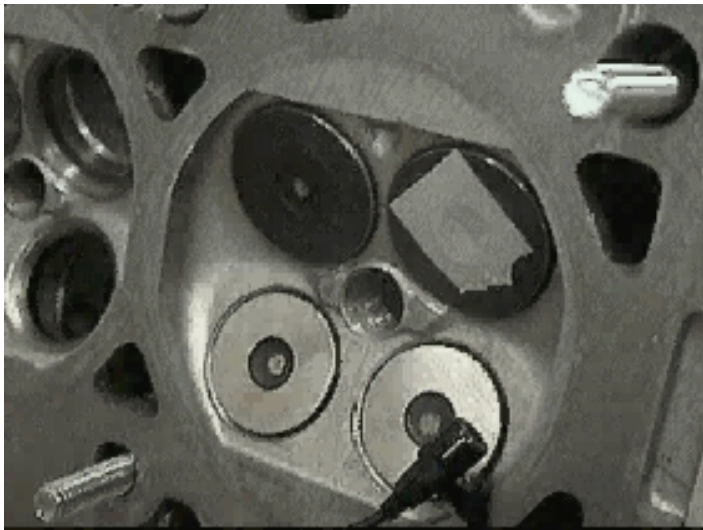
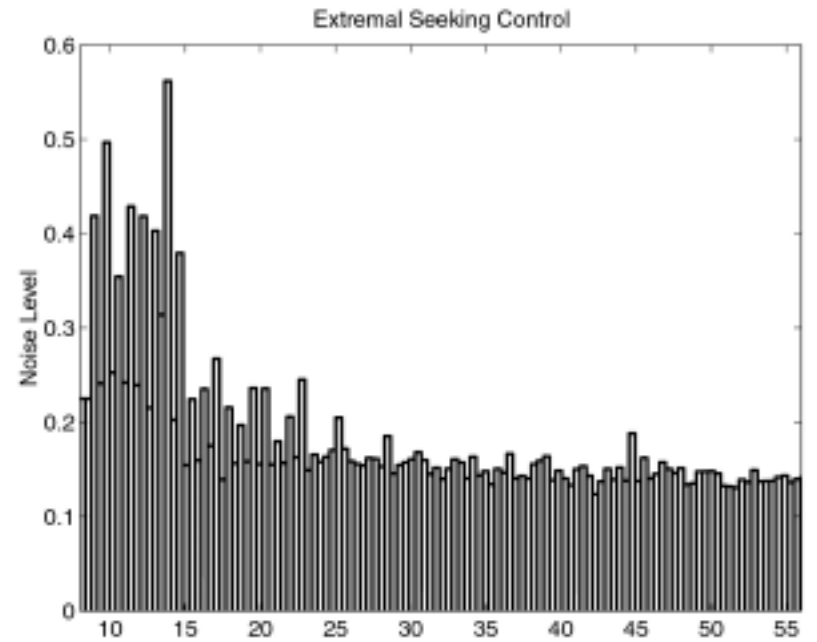
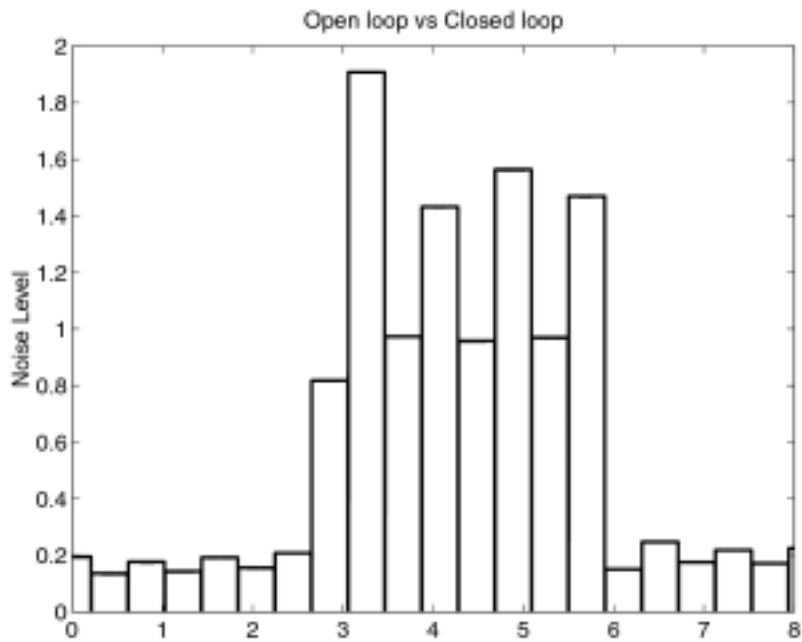
Impact Velocity

- Mean: 0.08 m/s
- σ : 0.05 m/s

Additional factor of 2 reduction

- Total of a factor of 12 reduction!!!!





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Conclusion and Future Work

- Conclusion:
 - A nonlinear controller were designed and implemented
 - Achieved a mean impact velocity of 0.16 m/s
 - Achieved consistent transition times of less than 4 ms
 - Factor of 6 reduction over open loop control
 - Extremal Seeking Control was applied to improve performance from cycle to cycle
 - Achieved a mean impact velocity of 0.08 m/s
 - Factor of 12 reduction over open loop control!!!!

- Future Work:
 - Study the affects of valve lash
 - Augment controller to account for disturbances caused by pressure differences across the valve



The question at hand: Will this control algorithm make camshafts obsolete??

